Results from the Phoenix Atmospheric Structure Experiment

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# Outline

- Overview of trajectory and atmospheric structure reconstruction for Phoenix
- Highlight selected aspects of Phoenix reconstruction that offer lessons for future missions
- Demonstration of real-time reconstruction technique using direct-to-Earth radio link (Opportunity EDL)

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# Phoenix atmospheric entry



JPL figure

- 25 May 2008
- Landing site at
  - 68.2N, 234.3E
  - -4.1 km (MOLA)
- Ls=77, LST ~16:30
- Ballistic entry with many similarities to Pathfinder and MER
- Accelerometers and gyroscopes on board
- IMU specifications, location, etc, etc fixed without scientific input
- 200 Hz data (good), but noisy (bad)

# 200 Hz accelerations



# **Smoothed accelerations**



# **Reconstructed trajectory**



Reconstruction process essentially same as used for Spirit and Opportunity, with exception of gyroscope data

> 5600 m/s to 6.1+-/3.6 m/s with design value of "few m/s"!

 Attitude found directly using gyroscopes, angle of attack is well behaved

- Parachute deployment at 13.5 km and 391 m/s (Mach 1.7)
- First ground contact at 1.10 +/- 1.49 km above ground level and 6.1 +/- 3.6 m/s

#### **Reconstructed thermal structure**



Reconstruction process essentially same as used for Spirit and Opportunity, but with updated aerodynamics and known attitude

- Much warmer than CO<sub>2</sub> condensation curve
- Mesopause
- Tides
- Gravity waves

# **Comparison with MCS profiles**



MCS = Mars Climate Sounder instrument on MRO

Good agreement at low altitudes, gets worse as altitude increases

Strong signature of diurnal thermal tide



# Gravity waves



Vertical wind speeds of ~5 m/s associated with these 5 K oscillations with 7 km wavelength

Comparison with general circulation models



#### Success of project's empirical model



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# Challenges for smoothing accelerations



Exponential increase at high altitudes

$$a = a_0 \exp \frac{t}{\tau}$$

Discontinuities appear when width of averaging window is changed



- Mean of an exponential function does not equal desired central value
- Can't use mean of log(a) because noisy data varies sign

# Solution – Use two averages

$$a_{mean} = \frac{1}{2t_X} \int_{t=-t_X}^{t=t_X} a_0 \exp\left(\frac{t}{\tau}\right) dt$$

$$a_{mean} = \frac{a_0 \tau}{2t_X} \left[ \exp \frac{t_X}{\tau} - \exp \frac{-t_X}{\tau} \right]$$

$$a_{mean} = a_0 \frac{\tau}{t_X} \sinh\left(\frac{t_X}{\tau}\right)$$

Calculate "long average" aL from t = -2ts to t = +2ts

$$a_L = a_0 \frac{\tau}{2t_S} \sinh\left(\frac{2t_S}{\tau}\right)$$
$$a_S = a_0 \frac{\tau}{t_S} \sinh\left(\frac{t_S}{\tau}\right)$$

$$\frac{a_L}{a_S} = \frac{1}{2} \frac{\sinh\left(\frac{2t_S}{\tau}\right)}{\sinh\left(\frac{t_S}{\tau}\right)}$$
$$\frac{a_L}{a_S} = \cosh\left(\frac{t_S}{\tau}\right)$$

Calculate "short average" aS from t = -ts to t = +ts

Ratio gives desired tau

$$\frac{t_S}{\tau} = \ln\left(\frac{a_L}{a_S} + \sqrt{\left(\frac{a_L}{a_S}\right)^2 - 1}\right)$$



Grey dots are normal smoothing with 1024 point running mean Black dots are normal smoothing with 2048 point running mean

Difference indicates the problem How do you transition from one averaging window to another?

Grey dots are 1024 point running mean corrected using ratio to 2048 point running mean Black dots are 2048 point running mean corrected using ratio to 4096 point running mean

Overlap of two series enables easy transition from one averaging window to the next

# Transformation from IMU frame into spacecraft frame

 $\underline{M}_{IMU}^{C} = \begin{pmatrix} 0.0016580000000 & 0.4345320000000 & 0.90065500000000 \\ 0.865583671733631 & -0.451637796435926 & 0.216304845776395 \\ 0.500761102355330 & 0.779233610045474 & -0.37687298280806 \end{pmatrix}$ 

One source, as built

M =	[	0	0.4226	0.9063]
	[	0.8660	-0.4532	0.2113 ]
	[	0.5	0.7849	-0.3660]

- Another source, as designed
- Differences seem small, but effects are not

# Effects of frames on trajectory



Differences of a few km in altitude at parachute deployment and landing, differences of tens of m/s in speed at landing

# Angle of attack



Results of two different methods for finding the angle of attack are inconsistent by 1-2 degrees. This is SEPARATE issue from predicted/reconstructed differences

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# Entry reconstructions – What if done in "real time"?

- Rapid estimate of landing site location
- Rapid assessment of accuracy of predicted environmental conditions
- Engage public during "EDL event"
- Don't need mission to survive after EDL for subsequent data transmission
- Direct-to-Earth radio link offers alternative approach

# Doppler shift during Opportunity EDL



This only gives one component of velocity. Assuming that the aerodynamic deceleration is parallel to velocity gives 3D velocity. Demonstrate using scanned version of this figure (not real data).

#### **Reconstructed trajectory**



#### **Reconstructed temperature**



Plausible temperatures between 20 km and 60 km. This technique works, but should be validated using real data. Uncertainty analysis also needed to estimate expected accuracy.

# Conclusions

- Trajectory and atmospheric structure reconstruction for Phoenix successful

   Results available in PDS
- Future atmospheric entry probes might consider:
  - Reduction of noise by smoothing
  - Sensitivity to mundane engineering details, like relationships between reference frames
  - Why two different angles of attack?
  - Potential of rapid reconstruction using radio link

# **Backup Material**

# Why bother?

- Independent reconstruction of trajectory
- Rapid results for:
  - Engineers (Where did we land? Nominal?)
  - Public (See results immediately)
  - Science (What are atmospheric conditions?)
- Get results even if lander explodes when reaching ground

## Detailed approach

Measured:
$$\underline{v} \cdot \underline{l_0}$$
Obvious: $\underline{v_1} = \underline{v_0} + \underline{a} \, dt$  $\underline{a} = \underline{a_{aero}} + \underline{g}$ Re-arrange: $\underline{v_1} \cdot \underline{l_0} = \underline{v_0} \cdot \underline{l_0} + \underline{a} \cdot \underline{l_0} \, dt$ Re-arrange: $\underline{a_{aero}} \cdot \underline{l_0} = \frac{1}{dt} \left( \underline{v_1} \cdot \underline{l_0} - \underline{v_0} \cdot \underline{l_0} \right) - \underline{g} \cdot \underline{l_0}$ 

**Big assumption:** 

$$\underline{a_{aero}} = -k\underline{v_0}$$

#### Outcome is expression for <u>a-aero</u> using known quantities

$$\underline{a_{aero}} = \frac{-\underline{v_0}}{\underline{v_0} \cdot \underline{l_0}} \left[ \frac{1}{dt} \left( \underline{v_1} \cdot \underline{l_0} - \underline{v_0} \cdot \underline{l_0} \right) - \underline{g} \cdot \underline{l_0} \right]$$